

(12) **United States Patent**  
**Koroglu et al.**

(10) **Patent No.:** **US 9,209,838 B2**  
(45) **Date of Patent:** **Dec. 8, 2015**

(54) **LOW-COST RECEIVER USING INTEGRATED INDUCTORS**

(71) Applicant: **Silicon Laboratories Inc.**, Austin, TX (US)

(72) Inventors: **Mustafa H. Koroglu**, Austin, TX (US);  
**Yu Su**, Austin, TX (US)

(73) Assignee: **SILICON LABORATORIES INC.**, Austin, TX (US)

(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **14/612,232**

(22) Filed: **Feb. 2, 2015**

(65) **Prior Publication Data**

US 2015/0147991 A1 May 28, 2015

**Related U.S. Application Data**

(60) Division of application No. 13/468,824, filed on May 10, 2012, now Pat. No. 8,983,417, which is a continuation-in-part of application No. 13/342,548, filed on Jan. 3, 2012, now Pat. No. 8,725,103.

(51) **Int. Cl.**  
**H04B 1/18** (2006.01)  
**H04B 1/00** (2006.01)  
(Continued)

(52) **U.S. Cl.**  
CPC ..... **H04B 1/005** (2013.01); **H03F 3/19** (2013.01); **H03H 7/0169** (2013.01); **H03H 7/46** (2013.01);  
(Continued)

(58) **Field of Classification Search**  
CPC ..... H03H 11/1291; H03H 11/1252; H03H 7/0153; H03H 2210/025; H03H 11/12; H03H 7/0169; H03H 7/09; H03H 7/38;

H04B 1/30; H04B 1/28; H04B 1/405; H04B 10/43; H04B 17/21; H04B 1/126; H04B 1/16; H04B 10/503; H04B 1/1027; H04B 1/1638; H04B 1/1684; H04B 1/18; H04B 1/44; H03F 1/02; H03F 1/26; H03F 2203/45008; H03F 3/45071

USPC ..... 455/130–355  
See application file for complete search history.

(56) **References Cited**

**U.S. PATENT DOCUMENTS**

2,080,560 A 5/1937 Case  
4,316,108 A 2/1982 Rogers, Jr.

(Continued)

**OTHER PUBLICATIONS**

“Applications of Switched-Capacitor Circuits in Active Filters and Instrumentation Amplifiers,” Dr. William R. Gris , Department of IET, Morehead State University, Technology Interface, vol. 3 No. 3, Fall 1999, ISSN# 1523-9926.

(Continued)

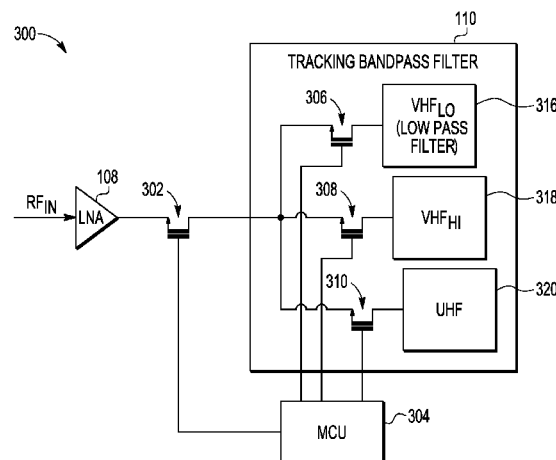
*Primary Examiner* — Lana N Le

(74) *Attorney, Agent, or Firm* — Polansky & Associates, P.L.L.C.; Paul J. Polansky

(57) **ABSTRACT**

A receiver includes a first amplifier having an input for receiving an RF signal, and an output for providing an amplified RF signal, a switch section that selectively switches the amplified RF signal onto a selected one of a plurality of nodes, and a filter section comprising a plurality of filters coupled to respective ones of the plurality of nodes. A first filter of the plurality of filters comprises a first variable capacitor coupled in parallel with an inductance leg between a corresponding one of the plurality of nodes and a power supply voltage terminal. The first variable capacitor has a capacitance that varies in response to a tuning signal. The inductance leg includes a first inductor in series with an effective resistance, wherein the effective resistance has a value related to an upper cutoff frequency to be tuned by the first filter.

**8 Claims, 7 Drawing Sheets**



- (51) **Int. Cl.**  
*H03J 3/10* (2006.01)  
*H04B 1/16* (2006.01)  
*H03H 7/01* (2006.01)  
*H03H 7/46* (2006.01)  
*H03H 11/12* (2006.01)  
*H03F 3/19* (2006.01)  
*H03H 7/09* (2006.01)
- (52) **U.S. Cl.**  
 CPC ..... *H03H 11/1291* (2013.01); *H03J 3/10* (2013.01); *H04B 1/16* (2013.01); *H04B 1/1638* (2013.01); *H04B 1/18* (2013.01); *H03F 2200/171* (2013.01); *H03F 2200/451* (2013.01); *H03H 7/09* (2013.01); *H03H 2210/025* (2013.01); *H03H 2210/033* (2013.01); *H03J 2200/32* (2013.01)
- (56) **References Cited**  
 U.S. PATENT DOCUMENTS
- |              |      |         |                                 |
|--------------|------|---------|---------------------------------|
| 4,361,909    | A    | 11/1982 | Theriault                       |
| 4,364,116    | A    | 12/1982 | Nossek                          |
| 4,368,541    | A    | 1/1983  | Evans                           |
| 4,408,348    | A    | 10/1983 | Theriault                       |
| 4,662,001    | A    | 4/1987  | Cruz                            |
| 5,577,235    | A    | 11/1996 | Mitra                           |
| 5,646,935    | A    | 7/1997  | Ishikawa et al.                 |
| 5,737,035    | A    | 4/1998  | Rotzoll                         |
| 6,097,273    | A    | 8/2000  | Frye                            |
| 6,177,964    | B1   | 1/2001  | Birleson et al.                 |
| 6,266,522    | B1   | 7/2001  | Holden                          |
| 6,377,315    | B1   | 4/2002  | Carr et al.                     |
| 6,377,788    | B1   | 4/2002  | Elder                           |
| 6,453,157    | B1   | 9/2002  | Roberts                         |
| 6,535,722    | B1   | 3/2003  | Rosen                           |
| 6,549,096    | B2   | 4/2003  | Groves et al.                   |
| 6,681,102    | B1   | 1/2004  | Collier                         |
| 6,778,117    | B1   | 8/2004  | Johnson                         |
| 6,813,485    | B2   | 11/2004 | Sorrells et al.                 |
| 6,915,114    | B2   | 7/2005  | Khorram                         |
| 6,917,328    | B2   | 7/2005  | Rabinowitz et al.               |
| 7,039,385    | B1   | 5/2006  | Hoffmann                        |
| 7,075,585    | B2   | 7/2006  | Favrat et al.                   |
| 7,095,454    | B2   | 8/2006  | Waight                          |
| 7,158,774    | B2   | 1/2007  | Helio                           |
| 7,231,192    | B2   | 6/2007  | Suzuki                          |
| 7,251,466    | B2   | 7/2007  | Porret et al.                   |
| 7,265,792    | B2   | 9/2007  | Favrat et al.                   |
| 7,305,223    | B2   | 12/2007 | Liu et al.                      |
| 7,327,406    | B2   | 2/2008  | Utsunomiya et al.               |
| 7,395,548    | B2   | 7/2008  | Runzo                           |
| 7,459,963    | B2   | 12/2008 | Kimura                          |
| 7,577,413    | B2   | 8/2009  | He                              |
| 7,620,379    | B2   | 11/2009 | Isaac                           |
| 7,869,780    | B2 * | 1/2011  | Youssofian et al. .... 455/222  |
| 7,899,431    | B2   | 3/2011  | Rahman et al.                   |
| 7,973,603    | B2   | 7/2011  | Kammula                         |
| 8,103,233    | B2   | 1/2012  | Im                              |
| 8,185,076    | B2   | 5/2012  | Miura et al.                    |
| 8,301,208    | B2   | 10/2012 | Katsube et al.                  |
| 8,653,886    | B2   | 2/2014  | Hellberg                        |
| 2001/0007151 | A1   | 7/2001  | Vorenkamp et al.                |
| 2003/0045263 | A1 * | 3/2003  | Wakayama et al. .... 455/323    |
| 2005/0040909 | A1   | 2/2005  | Waight                          |
| 2005/0070235 | A1 * | 3/2005  | Matsuura ..... 455/131          |
| 2006/0040628 | A1   | 2/2006  | Porret et al.                   |
| 2006/0064725 | A1   | 3/2006  | Rabinowitz et al.               |
| 2006/0078069 | A1   | 4/2006  | Seendripu et al.                |
| 2006/0223474 | A1 * | 10/2006 | Yoshizaki et al. .... 455/252.1 |
| 2007/0123176 | A1   | 5/2007  | Han et al.                      |
| 2007/0165143 | A1   | 7/2007  | Utsunomiya et al.               |
| 2008/0096508 | A1   | 4/2008  | Luff                            |
| 2008/0181337 | A1   | 7/2008  | Maxim                           |
| 2008/0198269 | A1   | 8/2008  | Gomez                           |
| 2009/0176467 | A1   | 7/2009  | Im                              |
| 2009/0251618 | A1   | 10/2009 | Gao                             |
| 2010/0097531 | A1   | 4/2010  | Miura et al.                    |
| 2010/0130155 | A1   | 5/2010  | Khoini-Poorfard                 |
| 2011/0098013 | A1   | 4/2011  | Takahashi et al.                |
| 2012/0302188 | A1   | 11/2012 | Sahota                          |
| 2012/0306588 | A1   | 12/2012 | Mcculloch et al.                |
| 2013/0095779 | A1 * | 4/2013  | Katsube et al. .... 455/232.1   |
| 2014/0106669 | A1   | 4/2014  | Krishnan et al.                 |
| 2014/0160608 | A1   | 6/2014  | Mo et al.                       |
- OTHER PUBLICATIONS
- “Novel LC Pseudo Switched Capacitor Filter Suited for Wireless RF Applications,” Ahmed El Oualkadi et al., IEICE Electronics Express, vol. 2, No. 8, Apr. 2005, pp. 286-291.
- Actions on the Merits for Copending U.S. Appl. No. 14/195,064, filed Mar. 3, 2014; Actions on the Merits for U.S. Appl. No. 13/468,824, filed May 10, 2012 which is the parent application of 1052-2108; and Actions on the Merits for U.S. Appl. No. 13/342,548, filed Jan. 3, 2012, which is the parent application of 1052-0108.
- \* cited by examiner

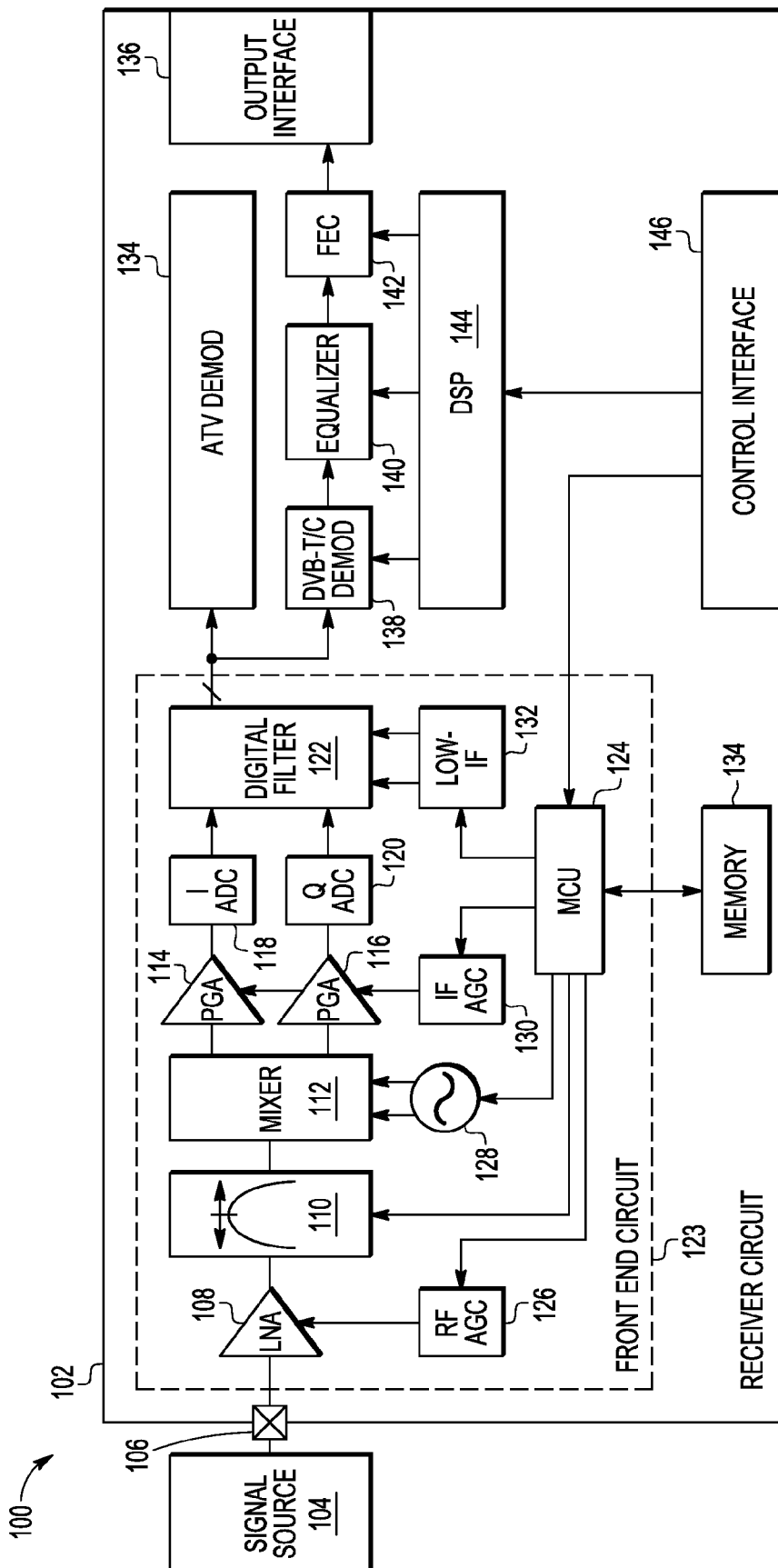


FIG. 1

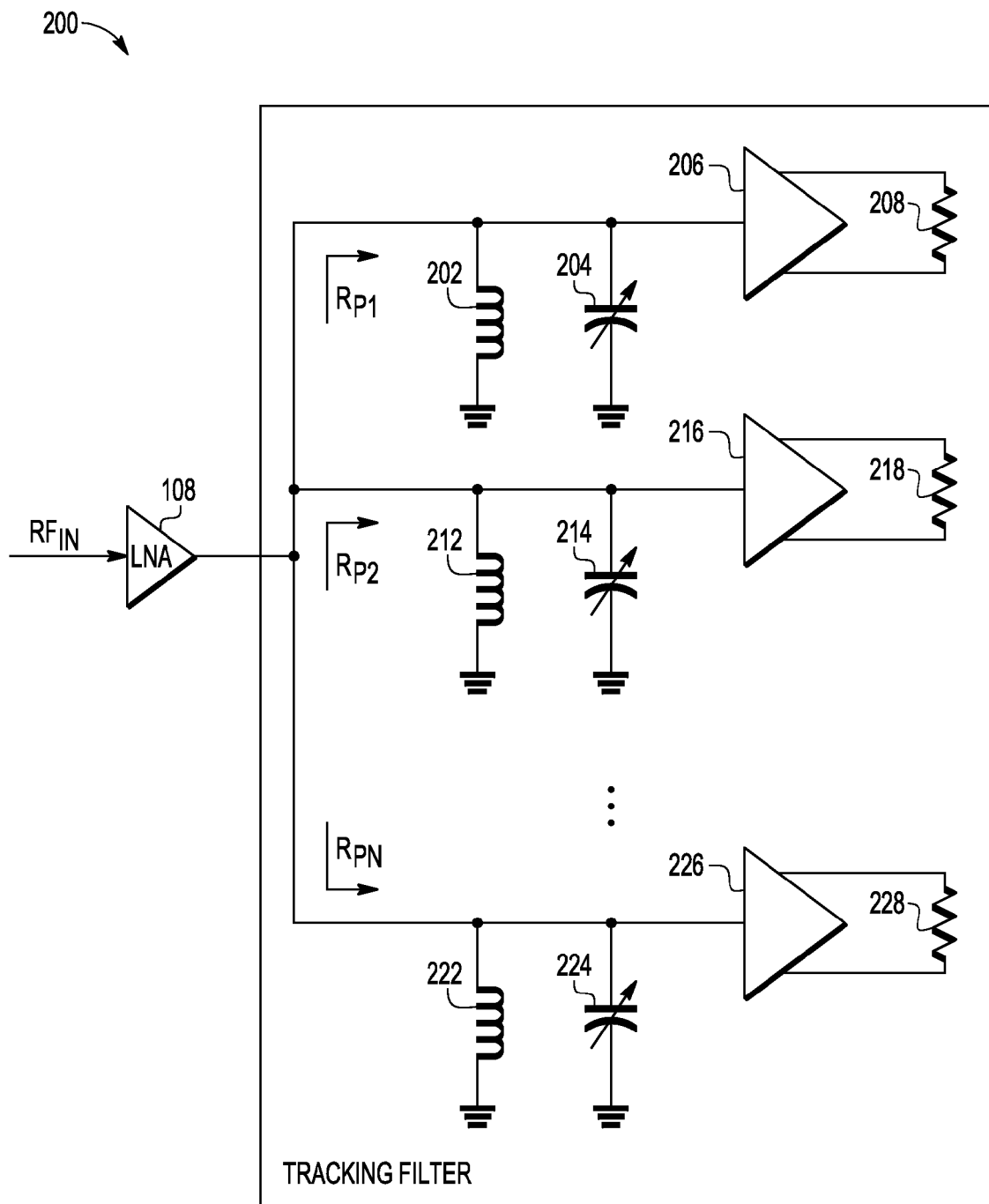


FIG. 2  
- PRIOR ART -

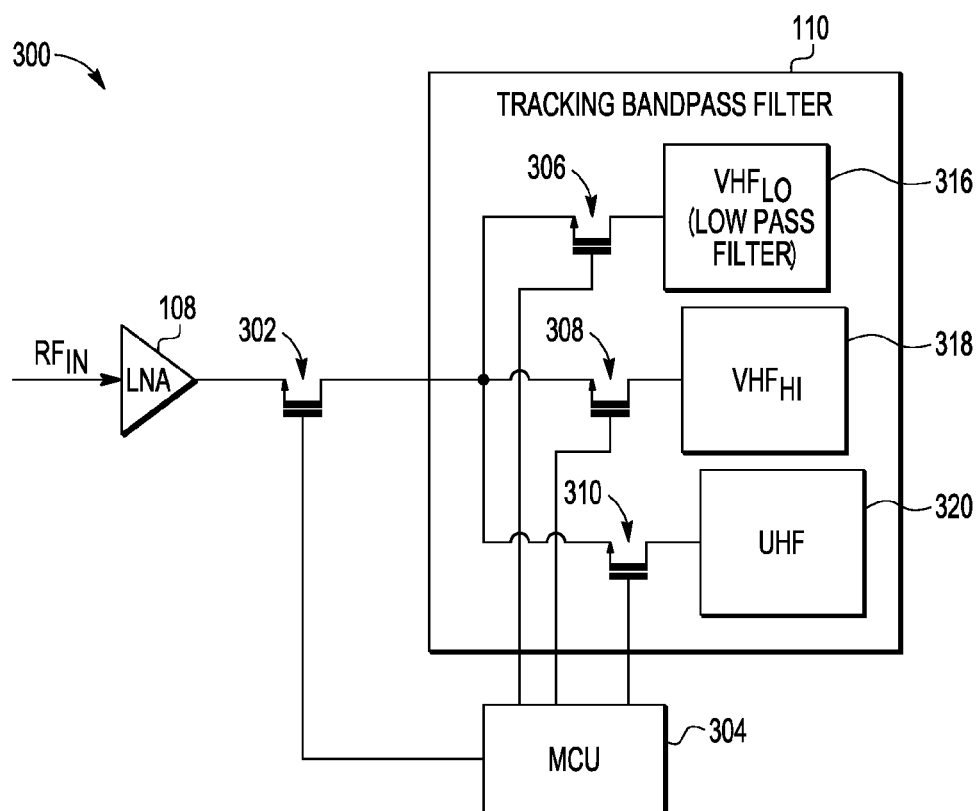


FIG. 3

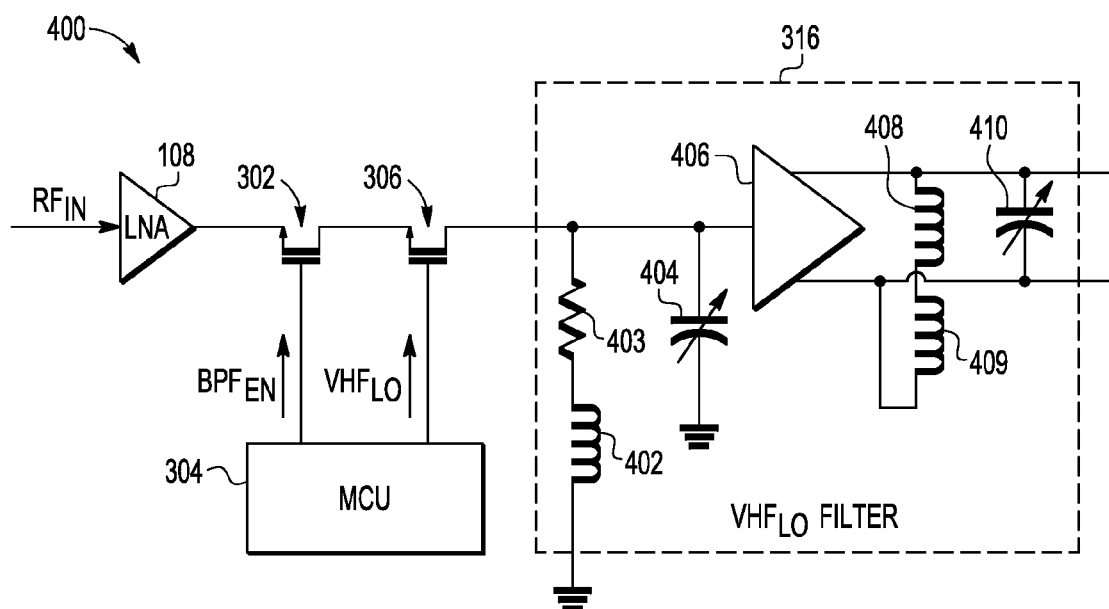


FIG. 4

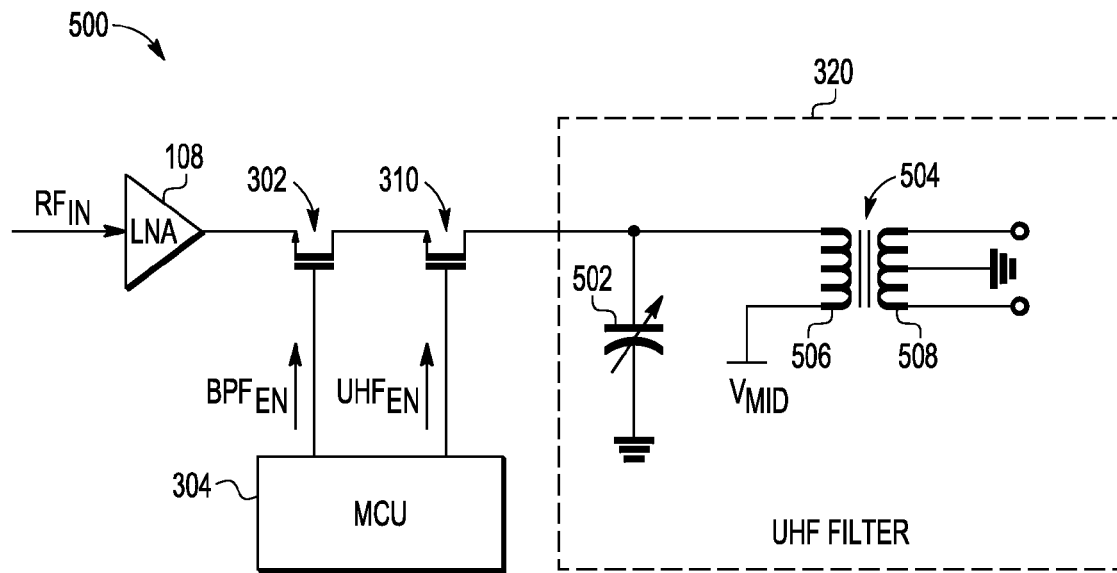


FIG. 5

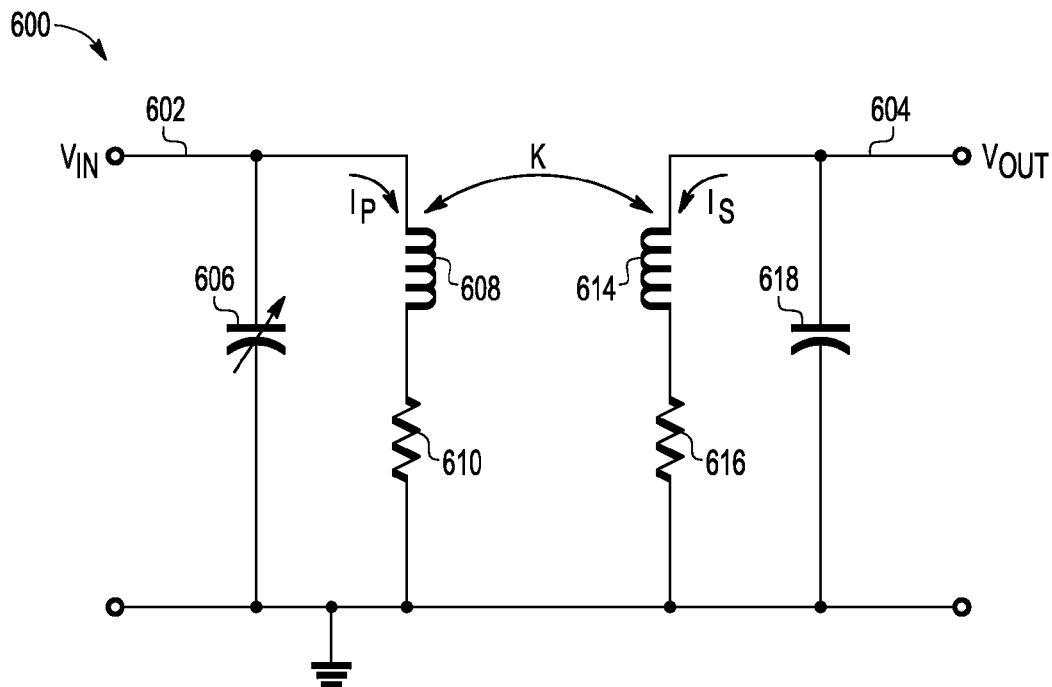


FIG. 6

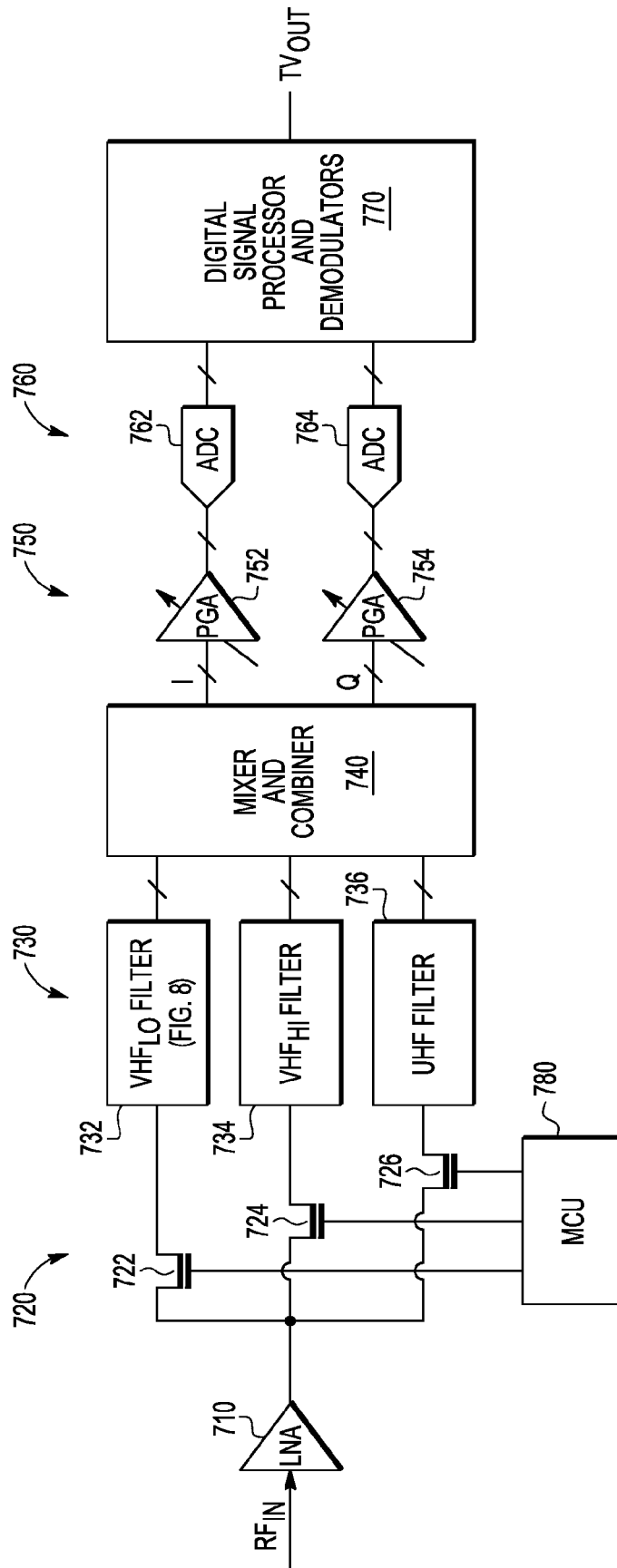
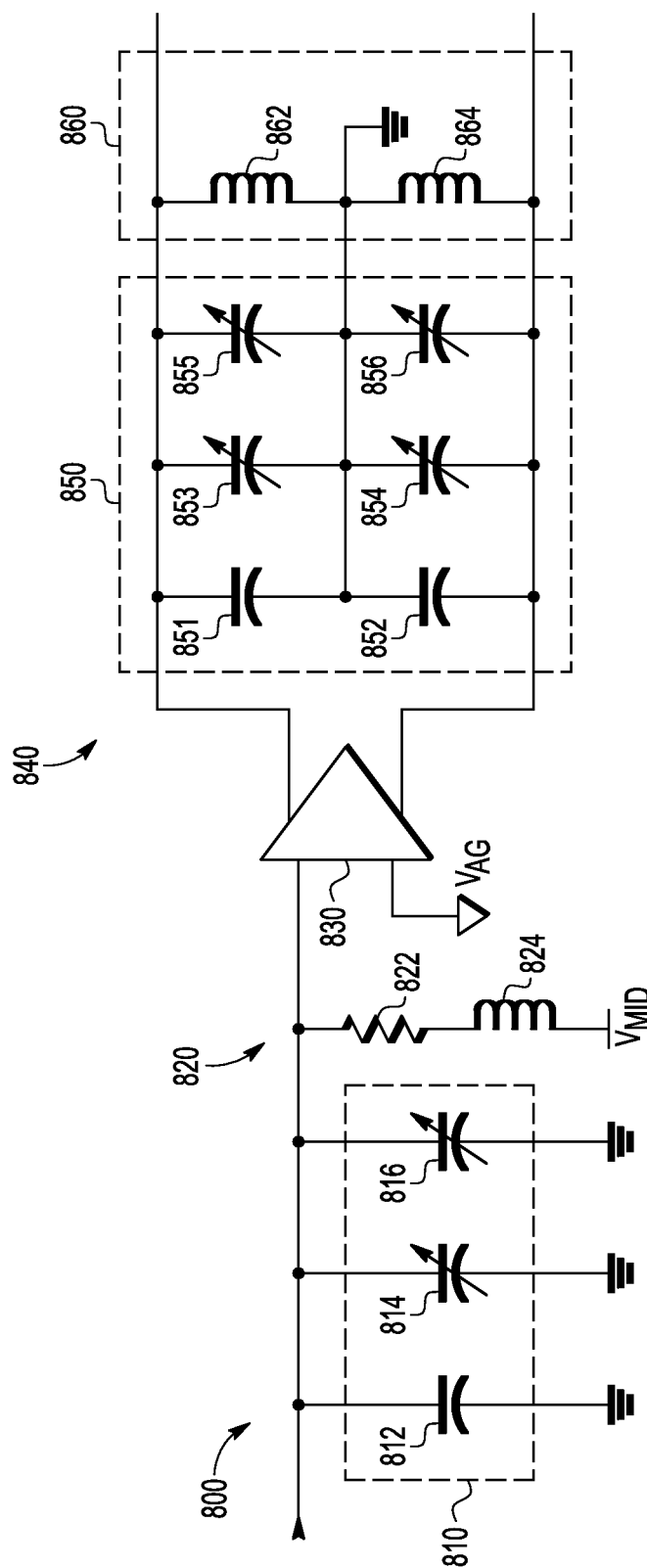


FIG. 7



732

FIG. 8



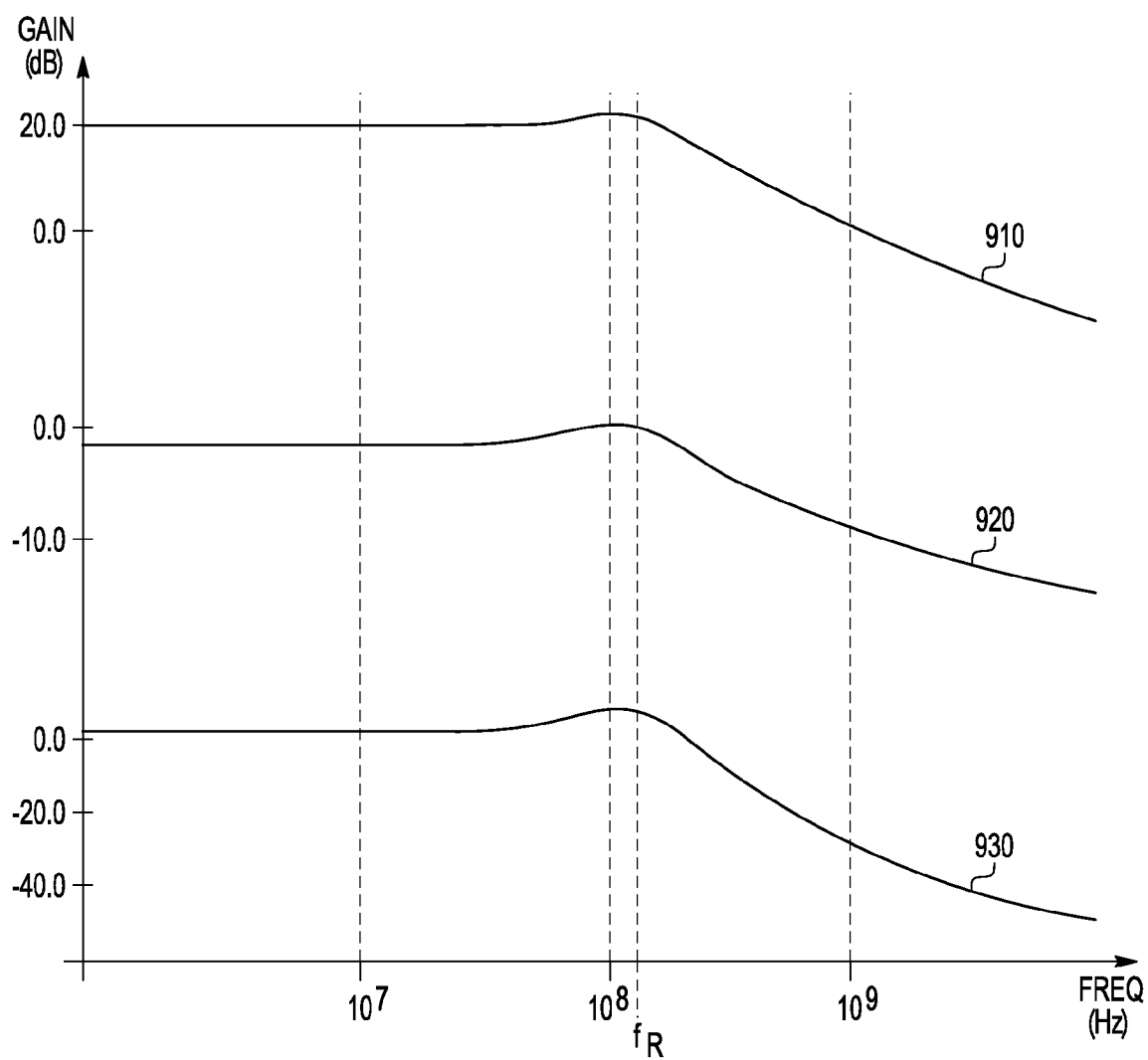


FIG. 9

## LOW-COST RECEIVER USING INTEGRATED INDUCTORS

This application is a division of prior application Ser. No. 13/468,824, which is a continuation-in-part of prior application Ser. No. 13/342,548, filed Jan. 3, 2012, entitled "Receiver Including a Tracking Filter," invented by Mustafa H. Koroglu and Yu Su.

### CROSS REFERENCE TO RELATED, CO-PENDING APPLICATION

Related subject matter is found in a copending patent application entitled "Integrated Receivers and Integrated Circuit Having Integrated Inductors and Method Therefor," application Ser. No. 14/195,064, invented by Ramin K. Poorfard, Alessandro Piovaccari, and Aslamali A. Rafi, filed Mar. 3, 2014 and assigned to the assignee hereof.

### FIELD OF THE DISCLOSURE

The present disclosure is generally related to receiver circuits, and more particularly to receiver circuits configurable to receive ultra high frequency and very high frequency broadcast radio frequency signals.

### BACKGROUND

Receiver circuits are used for both terrestrial and cable reception within televisions, digital video recorders, video cassette records, set-top box devices (such as cable and satellite tuners), frequency modulation (FM) radios, models, and other electronic devices. Some smart phones also utilize receiver circuits for television reception. In general, such receiver circuits include a tuner that selects a narrowband signal from within a wide or broad-band signal having multiple channels. The tuner includes bandpass filters, amplifiers, and mixer circuits for selecting a desired channel and for rejecting unwanted channels, noise and interference.

Television signals can be broadcast at a variety of different frequencies, including ultra-high frequency (UHF), very high frequency (VHF), and high frequency (HF) frequency bands. The International Telecommunications Union (ITU) defines the UHF frequency range as encompassing electromagnetic waves between 300 MHz and 3 GHz. VHF occupies frequencies within a range from approximately 30 MHz to 300 MHz, and HF occupies frequencies within a range from approximately 3 MHz to 30 MHz.

For a conventional tracking filter, multiple bandpass filters are included to cover the range of possible frequencies, each tuned to a limited portion of the overall bandwidth of the receiver. For each filter, a large tuned impedance is desirable to minimize the noise figure; however, the tuned impedance is typically a function of the frequency and the size of the inductor, which size can limit the frequency range for the particular filter.

Recently developed integrated circuit processes have allowed inductors to be built with sufficiently large inductance to be integrated with conventional signal processing circuitry on a common complementary-metal-oxide-semiconductor (CMOS) chip. However the inductors are relatively large, and to increase the inductance it may be necessary to either increase the size or decrease the quality factor of the inductor. A new receiver that is able to relax this tradeoff would be desirable.

## BRIEF DESCRIPTION OF THE DRAWINGS

The present disclosure may be better understood, and its numerous features and advantages made apparent to those skilled in the art by referencing the accompanying drawings, in which:

FIG. 1 is a block diagram of an embodiment of a system including a receiver circuit having a tracking filter configurable to receive VHF<sub>LO</sub>, VHF<sub>HI</sub>, and UHF broadcast signals.

FIG. 2 is a circuit diagram of a representative example of a receiver including conventional tracking filter having a separate bandpass filter tuned for each frequency band.

FIG. 3 is a block diagram of an embodiment of a portion of a receiver including a tracking bandpass filter having a VHF<sub>LO</sub> filter, a VHF<sub>HI</sub> filter, and a UHF filter.

FIG. 4 is a diagram of an embodiment of the VHF<sub>LO</sub> filter of FIG. 3.

FIG. 5 is a diagram of an embodiment of the UHF filter of FIG. 3.

FIG. 6 is an embodiment of a small signal model of the UHF Filter of FIG. 5.

FIG. 7 is a block diagram of a low-cost television receiver according to an embodiment of the present invention.

FIG. 8 illustrates in schematic form the VHF<sub>LO</sub> filter of FIG. 7.

FIG. 9 illustrates a frequency domain graph useful in understanding the operation of the VHF<sub>LO</sub> filter of FIG. 7.

The use of the same reference symbols in different drawings indicates similar or identical items.

### DETAILED DESCRIPTION

Embodiments of a receiver circuit are described below that include a low noise amplifier for receiving a radio frequency signal and including an output coupled to an input of a tracking filter configured to receive very high frequency (VHF<sub>LO</sub> and VHF<sub>HI</sub>) and UHF broadcast signals. As used herein, VHF<sub>LO</sub> signals refer to radio frequency signals in a range of approximately 50 to 190 MHz, VHF<sub>HI</sub> signals refer to radio frequency signals in a range of approximately 190 to 470 MHz, and UHF signals refer to radio frequency signals in a range of approximately 470 to 860 MHz. The VHF<sub>LO</sub> portion of the tracking filter includes a low pass filter for receiving VHF<sub>LO</sub> broadcast signals and that utilizes inductive peaking to extend an upper frequency range (or limit) of the low-pass filter. The VHF<sub>LO</sub> portion of the tracking filter includes a single-to-differential amplifier having an input coupled to the output of the low noise amplifier, and having a first output and a second output. The VHF<sub>LO</sub> portion of the tracking filter further includes a band-pass filter coupled between the first and second outputs, which band-pass filter can be an inductive-capacitive filter. The UHF portion of the tracking filter uses a transformer in place of a single-to-differential amplifier. The transformer includes a primary winding coupled to the output of the low noise amplifier and a secondary winding magnetically coupled to the primary winding. The secondary winding is configured to include more turns than the primary winding in order to provide a signal gain between the primary and secondary windings. An example of one possible embodiment of a receiver circuit having a filter configured for VHF<sub>LO</sub>, VHF<sub>HI</sub>, and UHF reception is described below with respect to FIG. 1.

FIG. 1 is a block diagram of an embodiment of a system 100 including a receiver circuit 102 having a tracking filter 110 configurable to receive VHF<sub>LO</sub>, VHF<sub>HI</sub>, and UHF broadcast signals. System 100 includes a signal source 104 coupled to receiver circuit 102 through an input terminal or pad 106.

Signal source **104** can be an antenna, a coaxial cable, or other signal source for delivering radio frequency broadcast signals to pad **106**. Receiver circuit **102** includes a front end circuit **123**, which includes a low-noise amplifier (LNA) **108** having an input coupled to pad **106** and an output coupled to an input of a tracking filter **110**. Tracking filter **110** includes a control input coupled to microcontroller unit **124** and an output coupled to an input of a mixer **112**.

Mixer **112** includes inputs for receiving an oscillator signal from a local oscillator **128**. Mixer **112** further includes an output for providing an in-phase signal to a programmable gain amplifier (PGA) **114** and an output for providing a quadrature signal to PGA **116**. PGA **114** includes an output coupled to an analog-to-digital converter (ADC) **118**, which has an output coupled to an input of a digital filter **122**. PGA **116** includes an output coupled to ADC **120**, which has an output coupled to an input of digital filter **122**.

Front end circuit **123** also includes a radio frequency automatic gain control (AGC) circuit **126** including an input coupled to an output of MCU **124** and an output coupled to an input of LNA **108**. MCU **124** is also coupled to local oscillator **128** to control the frequency of the local oscillator signals. Front end circuit **123** further includes an intermediate frequency (IF) AGC circuit **130** including a control input coupled to an output of MCU **124** and outputs coupled to PGAs **114** and **116**. Front end circuit **123** also includes a low-IF circuit **132** having a control input coupled to an output of MCU **124** and includes outputs coupled to inputs of digital filter **122**. MCU **124** is also coupled to memory **148**, which may store instructions and/or data that can be used by MCU **124** to control operation of the front end circuit **123**.

Receiver **102** further includes an analog television demodulator **134** having an input coupled to an output of digital filter **122** and an output coupled to an input of an output interface **136**. Receiver **102** also includes a digital video broadcast terrestrial/cable (DVB-T/C) demodulator **138** having an input coupled to the output of digital filter **122**, an input coupled to an output of digital signal processor (DSP) **144**, and an output coupled to an input of equalizer **140**. Equalizer **140** includes an input coupled to an output of DSP **144**, and an output coupled to an input of a forward error correction (FEC) circuit **142**, which has a second input coupled to an output of DSP **144** and an output coupled to an input of output interface **136**. DSP **144** includes a control input coupled to an output of a control interface **146**, which may be coupled to a host system for receiving control and other signals. Control interface **146** also includes an output coupled to MCU **124**.

Digital filter **122** provides the output signals to tuner circuitry, including analog television demodulator **134** and DVB-T/C demodulator **138**, which demodulate the video signal. Analog television demodulator **134** provides the demodulated output to output interface **136**, which may be coupled to an audio/video system on a chip or other multimedia circuit. DVB-T/C demodulator **138** provides the output to equalizer **140**, which adjusts the relative strength of selected frequencies within the demodulated output signal and provides the adjusted signal to FEC **142**. FEC **142** uses forward error correction to correct signal errors and provides the corrected signal to output interface **136**.

In this example, tracking filter **110** includes a low-pass filter portion for receiving and filtering VHF<sub>LO</sub> broadcast signals, a second filter portion for receiving and filtering VHF<sub>HI</sub> broadcast signals, and a third filter portion for receiving and filtering UHF broadcast signals. In an example, the low-pass filter portion includes a single-to-differential amplifier that includes an inductor/capacitor bandpass filter at the outputs and uses inductive peaking to extend the bandwidth

range. The third portion of the filter eliminates the single-to-differential amplifier and replaces it with a transformer having a primary winding with a relatively high quality factor (Q) and a secondary winding with a much lower Q. The transformer can provide approximately a 3 decibel (3 dB) gain. By introducing a gain between the primary and second windings, any impact of limited linearity of the output of LNA **108** on overall system linearity is also reduced.

By adjusting the VHF<sub>LO</sub> and UHF filter portions, the overall number of inductive-capacitive (LC) filters through the tracking filter **110** can be reduced. In an example, the frequency range over which the receiver **102** operates can be divided into an upper range, a mid-range, and a low range of frequencies, thereby reducing the overall complexity of the tracking filter.

In conventional tracking filters, the input impedance of each filter is often designed to be large to minimize the noise figure. To achieve the high tuned impedance, the size of the inductor is increased, which limits the maximum tuned frequency for each filter. Accordingly, a number of filters are included to provide filtering across the frequency range. A representative example of a receiver including a conventional tracking filter is described below with respect to FIG. 2.

FIG. 2 is a circuit diagram of a representative example of a receiver **200** including a conventional tracking filter **201** having a separate bandpass filter tuned for each frequency band. Receiver **200** includes LNA **108** having an input for receiving a radio frequency input signal (RF<sub>IN</sub>) and an output coupled to an input of tracking filter **201**.

Tracking filter **201** can include any number (N) of signal paths. In the illustrated example includes a first signal path including an inductor **202**, a variable capacitor **204**, a single-to-differential amplifier **206**, and a resistor **208**. Inductor **202** includes a first terminal coupled to the input of tracking filter **201** and a second terminal coupled to ground. Capacitor **204** includes a first electrode coupled to the input of tracking filter **201** and a second electrode coupled to ground. Single-to-differential amplifier **206** includes an input coupled to the input of tracking filter **201**, a first output coupled to a first terminal of resistor **208** and a second output coupled to a second terminal of resistor **208**.

Tracking filter **201** further includes a second signal path including an inductor **212**, a variable capacitor **214**, a single-to-differential amplifier **216**, and a resistor **218**. Inductor **212** includes a first terminal coupled to the input of tracking filter **201** and a second terminal coupled to ground. Capacitor **214** includes a first electrode coupled to the input of tracking filter **201** and a second electrode coupled to ground. Single-to-differential amplifier **216** includes an input coupled to the input of tracking filter **201**, a first output coupled to a first terminal of resistor **218** and a second output coupled to a second terminal of resistor **218**.

Tracking filter **201** also includes an N-th signal path including an inductor **222**, a variable capacitor **224**, a single-to-differential amplifier **226**, and a resistor **228**. Inductor **222** includes a first terminal coupled to the input of tracking filter **201** and a second terminal coupled to ground. Capacitor **224** includes a first electrode coupled to the input of tracking filter **201** and a second electrode coupled to ground. Single-to-differential amplifier **226** includes an input coupled to the input of tracking filter **201**, a first output coupled to a first terminal of resistor **228** and a second output coupled to a second terminal of resistor **228**.

In an example, resistors **208**, **218**, and **228** are approximately ninety ohm resistors and inductors **202**, **212**, and **222** have widths and lengths of approximately 600 μm×600 μm. The input impedances (R<sub>P1</sub>, R<sub>P2</sub>, . . . , and R<sub>PN</sub>) for each of the

5

signals paths (1 through N) is large enough to achieve a low noise factor. For some receivers, the input impedances between 400 Ohms and 800 Ohms. For tuned inductive LC filters, the tuned impedance is given by  $R_p = w_0 * L * Q$  where  $w_0$  is the resonant frequency, L is the inductance, Q is the quality factor, and  $R_p$  is the input impedance. For on-chip inductors, the quality factor (Q) is substantially constant for a given area and Q is proportional to the square root of the inductor area. To synthesize the desired impedance, the size of inductors 202, 212, and 222 is increased to improve Q or the inductance value is increased to avoid increased inductor area. However, large inductance values limit the maximum tuned frequency according to the following equation:

$$\omega_{\max} = \frac{1}{\sqrt{L_N * C_T}} \quad (1)$$

where the variable ( $C_T$ ) represents a total parasitic capacitance. Unfortunately, this limitation increases the number of filters that are included in tracking filter 201 in order to provide the desired channel tuning.

To reduce the number of signal paths and thus the number of LC filters, tracking filter 110 of FIG. 1 extends each transfer function to cover a wider frequency band, reducing the number of signal paths and thus reducing the complexity of the circuit. An example of a tracking filter that provides three transfer functions is described below with respect to FIG. 3.

FIG. 3 is a block diagram of an embodiment of a portion of a receiver 300 including a tracking filter 110 having a VHF<sub>LO</sub> filter 316, a VHF<sub>HF</sub> filter 318, and a UHF filter 320. Receiver 300 includes LNA 108 having an input for receiving a radio frequency input signal (RF<sub>IN</sub>) and an output coupled to a source of a transistor 302. Transistor 302 includes a gate coupled to an output of an MCU 304, and a drain coupled to an input of tracking filter 110. Tracking filter 110 includes a transistor 306 having a source coupled to the input of tracking filter 110, a gate coupled to MCU 304, and a drain coupled to an input of VHF<sub>LO</sub> filter 316, which is implemented as a low pass filter. Tracking filter 110 further includes a transistor 308 having a source coupled to the input of tracking filter 110, a gate coupled to MCU 304, and a drain coupled to an input of VHF<sub>HF</sub> filter 318. Tracking filter 110 also includes a transistor 310 having a source coupled to the input of tracking filter 110, a gate coupled to MCU 304, and a drain coupled to an input of UHF filter 320.

During operation, MCU 304 selectively enables the signal path between LNA 108 and one of the filters 316, 318, and 320. In an example, MCU 304 activates transistors 302 and 306 to provide the output of LNA 108 to the input of VHF<sub>LO</sub> filter 316. In this instance, the VHF<sub>LO</sub> filter 316 is a low-pass filter that passes frequencies within the tuning range from approximately 50 MHz to approximately 190 MHz. There are no television channels below a frequency of 50 MHz, thus VHF<sub>LO</sub> filter 316 can be configured to low pass filter operation. Toward the higher end of the range (i.e., as the frequency approaches approximately 190 MHz, the bandwidth of the VHF<sub>LO</sub> filter 316 is extended by using inductive peaking to extend the tuning range. An example of the VHF<sub>LO</sub> filter 316 illustrating one possible circuit configuration is described below with respect to FIG. 4.

FIG. 4 is a diagram of an embodiment of a receiver 400, such as receiver 300 in FIG. 3, including the VHF<sub>LO</sub> filter 316. VHF<sub>LO</sub> filter 316 includes an inductor 402 and a resistor 403. Resistor 403 has a first terminal coupled to the source of transistor 306 and has a second terminal coupled to a first

6

terminal of inductor 402, which has a second terminal coupled to ground. In this instance, resistor 403 represents the series resistance of inductor 402. VHF<sub>LO</sub> filter 316 further includes a variable capacitor 404 having a first electrode coupled to the drain of transistor 306 and a second electrode coupled to ground. VHF<sub>LO</sub> filter 316 also includes a single-to-differential amplifier 406 having a first output and a second output. Inductors 408 and 409 are connected in series between the first and second outputs. Additionally, a variable capacitor 410 includes a first electrode coupled to the first output and a second electrode coupled to the second output. The first and second outputs may be coupled to a load, such as a ninety ohm resistance.

In this example, the input impedance of VHF<sub>LO</sub> filter 316 is mostly provided by the series resistance of the inductor 402 at low frequencies. At higher frequencies, inductor 402 extends the bandwidth through inductive peaking. The quality factor requirements are relaxed substantially making it possible to use a smaller inductor. However, the smaller inductance and correspondingly smaller input impedance sacrifices some rejection at the higher and the lower side of the frequency band. To improve rejection, VHF<sub>LO</sub> filter 316 includes an inductive/capacitive (LC) bandpass filter at the outputs of the single-to-differential amplifier 406 using inductors 408 and 409 and variable capacitor 410. Instead of using a single 600  $\mu\text{m} \times 600 \mu\text{m}$  inductor, VHF<sub>LO</sub> filter 316 includes three 150  $\mu\text{m} \times 150 \mu\text{m}$  inductors, reducing the overall circuit area while extending the frequency range of VHF<sub>LO</sub> filter 316 relative to filters in tracking filter 201 in FIG. 2.

In the above example, VHF<sub>LO</sub> filter 316 from FIG. 3 uses an LC filter on the output of the single-to-differential amplifier to provide additional filtering. As the impedance level at the single-to-differential amplifier output is much smaller (about 90 Ohms), small-size, low-Q inductors can be used to implement the bandpass filter at the output of the single-to-differential amplifier. Thus, a high Q bandpass filter with a very large inductor is replaced by two lower-Q LC filters using much smaller inductors resulting in a reduced overall inductor area. The UHF filter 320 of FIG. 3 eliminates the active single-to-differential amplifier, reducing power consumption and improving the noise figure and linearity of the overall system. In place of the single-to-differential amplifier, UHF filter 320 introduces a transformer with a gain and with different Q factors between the primary and secondary inductive windings. By introducing a gain between the primary and secondary, the impact of the limited linearity of LNA 108 on overall system linearity is reduced. An example of a UHF filter 320 that uses a transformer instead of a single-to-differential amplifier is described below with respect to FIG. 5.

FIG. 5 is a diagram of an embodiment of a receiver 500 including the UHF filter 320 of FIG. 3. In this example, UHF filter 320 includes a variable capacitor 502 and a transformer 504. Variable capacitor 502 includes a first electrode coupled to the drain of transistor 310 and a second electrode coupled to ground. Transformer 504 includes a primary inductive winding 506 having a first terminal coupled to the drain of transistor 310 and a second terminal coupled to a supply voltage (such as a voltage approximately midway between the supply voltage rails, labeled " $V_{MID}$ "). Transformer 504 further includes a secondary inductive winding 508 having a first terminal and a second terminal, which can be coupled to mixer 112, and including a center tap coupled to ground.

In the illustrated example, the primary inductive winding 506 has a higher Q than the Q of the secondary inductive

7

winding **508**. Additionally, the transformer **504** introduces a gain from the primary inductive winding **506** to the secondary inductive winding **508**. In one instance, the gain is approximately 3 dB. In an example, the secondary inductive winding **508** of transformer **504** has more turns than the primary inductive winding **506**, providing the gain.

In a particular embodiment, the primary inductive winding **506** is formed from approximately 3.4  $\mu\text{m}$  of high quality copper (Cu), such as Cu M8, and approximately 2.8  $\mu\text{m}$  of aluminum (Al). In this embodiment, the secondary inductive winding **508** is formed from lower quality metal, such as Cu M4 or M5 and each has approximately 0.2  $\mu\text{m}$  of Cu. The primary and secondary inductive windings **506** and **508** can be patterned in redistribution layers of the semiconductor substrate. The secondary inductive winding **508** is formed from lower metals to improve the self-resonant frequency response of transformer **504**. Further, the coupling coefficient is very strong (approximately  $k=1$ ). A small signal model of an example of the UHF filter **320** is described below with respect to FIG. 6.

FIG. 6 is an embodiment of a small signal model **600** of the UHF Filter of FIG. 5. Small signal model **600** includes an input voltage terminal **602** for receive an input voltage ( $v_{in}$ ) and an output voltage terminal **604** for providing an output voltage ( $v_{out}$ ). Small signal model **600** includes variable capacitor **606** coupled between input voltage terminal **602** and ground. Variable capacitor **606** may represent variable capacitor **502** in FIG. 5 as well as a parasitic capacitance of the primary winding **506** of transformer **504** in FIG. 5. Small signal model **600** further includes an inductor **608** and a resistor **610** connected in series between input voltage terminal **602** and ground. Secondary winding **508** of transformer **504** in FIG. 5 is modeled as an inductor **614** and a resistor **616** connected in series between output voltage terminal **604** and ground. Additionally, a secondary capacitor **618** is coupled between output voltage terminal **604** and ground.

Assuming that the primary inductive winding **506** is tuned to a resonant frequency ( $\omega_0$ ) while the secondary inductive winding **508** is not tuned, resonant frequency of the secondary winding ( $\omega_s$ ) is much greater than the resonant frequency ( $\omega_0$ ) as follows:

$$\omega_s = \frac{1}{\sqrt{L_{614}C_{618}}} \quad (2)$$

where  $L_{614}$  represents the inductance of inductor **614** and  $C_{618}$  represents the capacitance of capacitor **618**. The coupling between the primary and the secondary inductive windings **506** and **508** is very strong ( $k$  is approximately equal to 1). The current into the secondary winding ( $i_s$ ) is determined according to the following equation:

$$i_s = \frac{-j\omega M i_p}{\frac{1}{j\omega C_{618}} + j\omega L_{614} + R_{616}} = -j\omega M i_p \frac{1}{\frac{1 - \omega^2 L_{614} C_{618}}{j\omega C_{618}} + R_{616}} \quad (3)$$

wherein  $R_{616}$  represents the resistance of resistor **616**, the frequency ( $\omega$ ) represents the input frequency, and the variable ( $M$ ) is determined by the following equation:

$$M = k\sqrt{L_{608}L_{614}} \quad (4)$$

8

Since  $k=1$ , for frequencies around the resonant frequency ( $\omega_0$ ), the current into the secondary winding **508** can be determined according to the following equation:

$$i_s = i_p \frac{\omega^2 M C_{614}}{1 + j\omega R_{616} C_{618}} \quad (5)$$

where  $i_s$  is the current flowing in the secondary inductive winding **508** and  $i_p$  is the current flowing in the primary inductive winding **506**.

In the illustrated example, the input voltage ( $v_{in}$ ) is determined by the following equation:

$$v_{in} = (j\omega L_{608} + R_{610})i_p + j\omega M \frac{\omega^2 M C_{618}}{1 + j\omega R_{616} C_{618}} i_p \quad (6)$$

and the effective impedance ( $Z_{eff}$ ) looking into the primary winding of the transformer is determined as follows:

$$Z_{eff} = \frac{v_{in}}{i_p} = j\omega L_{608} + R_{610} + \omega^2 M^2 \frac{j\omega C_{618}}{1 + j\omega R_{616} C_{618}} \quad (7)$$

In the equation 7, the factor  $j\omega L_{608} + R_{610}$  is the impedance due to the primary inductive winding **506**, and the remainder of the equation is the impedance due to the secondary inductive winding **508**. Assuming that the factor  $\omega R_{616} C_{618}$  is much smaller than 1, the effective impedance ( $Z_{eff}$ ) simplifies as follows:

$$Z_{eff} = j\omega L_{608} + R_{610} + \omega^2 M^2 j\omega C_{618} (1 - j\omega R_{616} C_{618}) = j\omega (L_{608} + \omega^2 M^2 C_{618}) + R_{610} + \omega^4 M^2 C_{618}^2 R_{616} \quad (8)$$

The effective impedance due to the inductance ( $L_{eff}$ ) is determined according to the following equation:

$$L_{eff} = L_{608} + \omega^2 M^2 C_{618} = L_{608} (1 + \omega^2 L_{614} C_{618}) = L_{608} \left(1 + \frac{\omega^2}{\omega_s^2}\right) \quad (9)$$

The effective impedance due to the resistance ( $R_{eff}$ ) is determined according to the following equation:

$$R_{eff} = R_{610} + \omega^4 M^2 C_{618}^2 R_{616} = R_{610} + \left(\frac{\omega}{\omega_s}\right)^4 \frac{L_{608}}{L_{614}} R_{616} \quad (10)$$

In the above examples, if the ratio of the resonant frequency ( $\omega_0$ ) to the frequency ( $\omega_s$ ) is kept small, the secondary inductive winding **508** has limited effect on the tuned frequency of primary inductive winding **506**. Additionally, by keeping this ratio small, the effect of the secondary inductive winding on the quality factor ( $Q$ ) is also kept small. For example, if the ratio is approximately  $1/3^{rd}$ , and the resistance ( $R_{616}$ ) is approximately 10 times the resistance of resistor **610**, and if the inductances of inductors **608** and **614** are approximately equal, then the effective quality factor ( $Q_{eff}$ ) can be determined by the following equation:

$$Q_{eff} \approx 0.99 \frac{\omega L_{608}}{R_{610}} \quad (11)$$

Further, on the secondary side, the output voltage ( $v_{out}$ ) relates to the input voltage ( $v_{in}$ ) according to the following equation:

$$v_{out} = v_{in} \sqrt{\frac{L_{614}}{L_{608}}} \quad (12)$$

Equation 12 demonstrates a conversion gain in transformer **504**. At higher frequencies, it can be demonstrated that the secondary inductive winding **508** acts as a second order inductive/capacitive (LC) low-pass filter on top of the LC bandpass characteristics of the primary inductive winding **506**.

Thus, the single-ended to differential conversion provided by a single-to-differential amplifier in the prior art can be replaced by performing the conversion magnetically with a transformer **504** having a secondary inductive winding **508** with a low quality factor. The effect of the secondary inductive winding **508** on the quality factor of the primary inductive winding **506** is proportional to the fourth power of the frequency. Accordingly, the quality factor and hence the gain of the LNA **108** decreases with increased tuned frequency, which helps to reduce the gain variation in the transfer function of the UHF filter **320**. Further, as discussed, it is possible to implement a conversion gain of more than 0 dB by adjusting a number of turns on the secondary inductive winding **508** to provide the gain. By introducing such a gain, the transformer **504** operates to reduce the signal level at the output of LNA **108**, improving the in-band third-order intercept point (IIP3) of the LNA **108** by providing the gain in the transformer **504**.

In conjunction with the circuits described above with respect to FIGS. 1-6, a receiver is disclosed that includes a tracking filter having a reduced number of LC filters relative to conventional tracking filters for television reception. In particular, the tracking filter divides the frequency range into three bands (VHF<sub>LO</sub>, VHF<sub>HI</sub>, and UHF), and provides a low-pass filter for the VHF<sub>LO</sub> frequencies, a bandpass filter for the VHF<sub>HI</sub> frequencies, and a transformer-based bandpass filter for UHF broadcast signals.

FIG. 7 is a block diagram of a low-cost television receiver **700** according to an embodiment of the present invention. Receiver **700** includes generally a low noise amplifier (LNA) **710**, a switch section **720**, a filter section **730**, a mixer and combiner **740**, an amplifier section **750**, an analog-to-digital converter (ADC) section **760**, a digital signal processor and demodulator section **770**, and a microcontroller **780**.

LNA **710** has an input for receiving input signal RF<sub>IN</sub>, and an output for providing an amplified RF<sub>IN</sub> signal. Switch section **720** includes three N-channel transistors **722**, **724**, and **726**. Transistor **722** has a first source/drain terminal connected to the output of LNA **710**, a gate, and a second source-drain terminal. Transistor **724** has a first source/drain terminal connected to the output of LNA **710**, a gate, and a second source-drain terminal. Transistor **726** has a first source/drain terminal connected to the output of LNA **710**, a gate, and a second source-drain terminal.

Filter section **730** includes a first filter labeled "VHF<sub>LO</sub> FILTER" **732**, a second filter labeled "VHF<sub>HI</sub> FILTER" **734**, and a third filter labeled "UHF FILTER" **736**. Filter **732** has an input connected to the second terminal of transistor **722**, a tuning input, and an output for providing a filtered differential signal. Filter **734** has an input connected to the second terminal of transistor **724**, a tuning input, and an output for providing a filtered differential signal. Filter **736** has an input con-

nected to the second terminal of transistor **726**, a tuning input, and an output for providing a filtered differential signal.

Mixer and combiner **740** has inputs connected to respective outputs of filters **732**, **734**, and **736**, a first output for providing a differential in-phase signal labeled "I", and a second output for providing a differential quadrature signal labeled "Q".

Amplifier section **750** includes programmable gain amplifiers (PGAs) **752** and **754**. PGA **752** has a differential input coupled to the first output of mixer and combiner **740**, a gain control input, and a differential output. PGA **754** has a differential input coupled to the second output of mixer and combiner **740**, a gain control input, and a differential output.

ADC section **760** includes ADCs **762** and **764**. ADC **762** has a differential input connected to the output of PGA **752**, and a multi-bit digital output. ADC **764** has a differential input connected to the output of PGA **754**, and a multi-bit digital output.

Digital signal processor and demodulator **770** has a first input connected to the output of ADC **762**, a second input connected to the output of ADC **764**, and an output for providing a signal labeled "TV<sub>OUT</sub>".

MCU **780** has a first output connected to the gate of transistor **722**, a second output connected to the gate of transistor **724**, a third output connected to the gate of transistor **726**, and a set of outputs not specifically shown in FIG. 7 connected to various other blocks as will be described further below.

In operation, receiver **700** is part of a highly integrated low-cost television receiver. LNA **710** receives the RF<sub>IN</sub> signal from an antenna or other signal source (not shown in FIG. 7), and provides the amplified RF<sub>IN</sub> signal to a selected one of three signal processing paths depending on the frequency band of the desired channel. In response to a tuning input (not shown in FIG. 7), MCU **780** under the control of firmware selects the appropriate signal processing path by activating one of the signals driving the gates of transistors **722**, **724**, and **726**. In receiver **700**, if the desired channel falls in the 50-190 MHz range, then MCU **780** activates the signal to the gate of transistor **722** and receiver **700** forms TV<sub>OUT</sub> from the amplified RF<sub>IN</sub> signal using VHF<sub>LO</sub> filter **732**. If the desired channel falls in the 190-470 MHz range, then MCU **780** activates the signal to the gate of transistor **724** and receiver **700** forms TV<sub>OUT</sub> from the amplified RF<sub>IN</sub> signal using VHF<sub>HI</sub> filter **734**. Filter **734** is a parallel resonant LC filter and includes a single-ended to differential converter. If the desired channel falls in the 470-860 MHz range, then MCU **780** activates the signal to the gate of transistor **726** and receiver **700** forms TV<sub>OUT</sub> from the amplified RF<sub>IN</sub> signal using UHF filter **736**. Filter **736** is implemented as described with respect to FIGS. 5 and 6 above.

Receiver **700** is suitable for very low cost applications by using several techniques. First, receiver **700** is fully integrated onto a single integrated circuit chip without expensive external components by using on-chip inductors now available in state-of-the-art CMOS processes. Second, filter section **730** uses only three bands instead of the five bands that receiver **200** of FIG. 2 uses. Third, UHF filter **736** uses an on-chip transformer in conjunction with a variable capacitor to accomplish both bandpass filtering as well as single-ended to differential conversion, thus saving circuit area required by an additional amplifier as well as improving the dynamic range of receiver **700**.

Fourth, VHF<sub>LO</sub> filter **732** uses a low-Q RLC filter and a low-Q LC bandpass filter that are smaller in area than a conventional parallel resonant LC filter, while providing most of the benefits of such a filter. The construction and characteristics of this filter will now be described.

## 11

FIG. 8 illustrates in schematic form VHF<sub>LO</sub> filter 732 of FIG. 7. Filter 732 includes generally an RLC lowpass filter 800, an amplifier 830, and a bandpass filter 840. Filter 800 includes a variable capacitor 810 and an inductance leg 820. Variable capacitor 810 includes a fixed capacitor 812, a binary-coded capacitor 814, and a thermometer-coded capacitor 816. Fixed capacitor 812 has a first terminal for receiving the amplified RF<sub>IN</sub> signal, and a second terminal connected to ground. Binary-coded capacitor 814 has a first terminal for receiving the amplified RF<sub>IN</sub> signal, a second terminal connected to ground, and a tuning input terminal for receiving a binary-coded tuning signal. Thermometer-coded capacitor 816 has a first terminal for receiving the amplified RF<sub>IN</sub> signal, a second terminal connected to ground, and a tuning input terminal for receiving a thermometer-coded tuning signal. Inductance leg 820 includes a resistor 822 and an inductor 824. Resistor 822 has a first terminal for receiving the amplified RF<sub>IN</sub> signal, and a second terminal. Inductor 824 has a first terminal connected to the second terminal of resistor 822, and a second terminal connected to V<sub>MID</sub>.

Amplifier 830 has a first input terminal for receiving the amplified RF<sub>IN</sub> signal, a second input terminal connected to a voltage labeled "V<sub>AG</sub>", and first and second output terminals for providing a differential output signal pair. V<sub>AG</sub> is an analog ground voltage that is nominally halfway between the more-positive and ground.

Bandpass filter 840 includes a variable capacitor 850, and a differential inductor 860. Variable capacitor 850 includes two fixed capacitors 851 and 852, two binary-coded capacitors 853 and 844, and two thermometer-coded capacitors 855 and 856. Capacitor 851 has a first terminal connected to the first output terminal of amplifier 830, and a second terminal connected to ground. Capacitor 852 has a first terminal connected to ground, and a second terminal connected to the second output terminal of amplifier 830. Capacitor 853 has a first terminal connected to the first output terminal of amplifier 830, a second terminal connected to ground, and a tuning input terminal for receiving a binary-coded tuning signal. Capacitor 854 has a first terminal connected to ground, a second terminal connected to the second output terminal of amplifier 830, and a tuning input terminal for receiving the binary-coded tuning signal. Capacitor 855 has a first terminal connected to the first output terminal of amplifier 830, a second terminal connected to ground, and a tuning input terminal for receiving a thermometer-coded tuning signal. Capacitor 856 has a first terminal connected to ground, a second terminal connected to the second output terminal of amplifier 830, and a tuning input terminal for receiving a thermometer-coded tuning signal.

Differential inductor 860 includes inductors 862 and 864. Inductor 862 has a first terminal connected to the first output terminal of amplifier 830, and a second terminal connected to V<sub>AG</sub>. Inductor 864 has a first terminal connected to V<sub>AG</sub>, and a second terminal connected to the second output terminal of amplifier 830.

In operation, filter 732 operates as a band filter and single-ended to differential converter for the amplified RF<sub>IN</sub> signal when the user selects a channel in the VHF<sub>LO</sub> band from 50 MHz to 190 MHz. However instead of merely providing a variable cutoff frequency within this band, lowpass filter 732 provides some selectivity in a narrower frequency band centered around the desired channel. Thus lowpass filter 732 provides some of the benefit of a bandpass filter without requiring high-quality (and thus large) on-chip inductors. At the same time, filter 732 significantly attenuates higher frequency components which helps maintain good signal-to-

## 12

noise ratio that might otherwise cause parasitic mixing of unwanted energy into the passband.

The resonant frequency of filter 800 ("f<sub>R</sub>") is given by:

$$f_R = \frac{1}{2\pi} \sqrt{\left(\frac{1}{LC}\right) \cdot \sqrt{1 + \frac{2R^2C}{L}} - \left(\frac{R}{L}\right)^2} \quad (13)$$

in which L represents the inductance of inductor 824, C represents the capacitance of variable capacitor 810, and R represents the resistance of resistor 822. The 3 dB bandwidth around f<sub>R</sub> ("BW") is given by:

$$BW = \frac{1}{2\pi} \cdot \frac{R}{L} \quad (14)$$

TABLE I below shows the values of the various components used in RLC filter 800 for the VHF<sub>LO</sub> filter band:

TABLE I

Element	Value
Fixed capacitor 812	1.63 pF
Binary coded capacitor 814	15 × 9.4 fF
Thermometer coded capacitor 816	31 × 150 fF
Resistor 822	396 Ω
Inductor 824	465 nH

in which pF represents picoFarads, fF represents femtoFarads, Ω represents ohms, and nH represents nanoHenrys. Note that the 396Ω resistance of resistor 822 is formed by 345Ω of parasitic resistance of inductor 824 along with a separate 54Ω resistor.

TABLE II below shows the values of the various components in bandpass filter 840 used for the VHF<sub>LO</sub> filter band:

TABLE II

Element	Value
Fixed capacitors 851 and 852	10 pF
Binary coded capacitors 853 and 854	15 × 150 fF
Thermometer coded capacitors 855 and 856	31 × 2.4 pF
Parasitic resistance of inductors 862 and 864	28 Ω
Inductors 862 and 864	86 nH

Using a currently available 0.55 micron CMOS manufacturing process with copper metallization and eight available metal layers, in VHF<sub>LO</sub> filter 732, inductor 824 can be formed in a die surface area of 150 microns (μm)×150 μm, and inductor 860 in a die surface area of 280 μm×160 μm. However as noted above the inductor in the VHF<sub>LO</sub> bandpass filter of receiver 200 of FIG. 2 requires a die surface area of approximately 600 μm×600 μm. Thus the lower-Q inductors used in VHF<sub>LO</sub> filter 732 require only about 19% of the die surface area of the higher-Q inductor required for the VHF<sub>LO</sub> bandpass filter of FIG. 2. Filter 732 actually takes advantage of the parasitic resistance in inductor 824 to reduce the size of the other components for a given f<sub>R</sub>. Thus filter 732 achieves most of the benefit of a parallel resonant bandpass filter but with significantly reduced die area and helps receiver 700 achieve low cost.

FIG. 9 illustrates a frequency domain graph useful in understanding the operation of the VHF<sub>LO</sub> filter of FIG. 7. In FIG. 9, the vertical axis represents gain in decibels (dB),

## 13

whereas the horizontal axis represents frequency on a logarithmic scale in Hz. A first waveform **910** corresponds to the frequency response of RLC filter **800** and is relatively flat but with a small dip of about 2-3 dB below  $f_R$ , exhibits a relatively constant dropoff with increasing frequency for frequencies above  $f_R$ , and has a peak at resonant frequency  $f_R$ . The peak is small for  $f_R$  near the low end of the VHF<sub>LO</sub> band, but increases to about 6 dB for  $f_R$  at the high end of the VHF<sub>LO</sub> band (the case illustrated in FIG. 9).

A second waveform **920** corresponds to the frequency response of bandpass filter **840**, and is substantially flat for lower frequencies below  $f_R$ , exhibits a relatively constant dropoff with increasing frequency for frequencies above  $f_R$ , and has a peak of about 4-6 dB at resonant frequency  $f_R$ . The peak is around 4 dB for  $f_R$  near the low end of the VHF<sub>LO</sub> band, and increases to about 6 dB for  $f_R$  at the high end of the VHF<sub>LO</sub> band.

A third waveform **930** corresponds to the overall frequency response to VHF<sub>LO</sub> filter **732**, and is relatively flat with a small dip for frequencies below  $f_R$ , exhibits a relatively constant dropoff with increasing frequency for frequencies above  $f_R$ , and has a peak of 4-10 dB at resonant frequency  $f_R$ . The peak is around 4 dB for  $f_R$  near the low end of the VHF<sub>LO</sub> band, and increases to about 10 dB for  $f_R$  at the high end of the VHF<sub>LO</sub> band. Thus the addition of bandpass filter **840** ensures some selectivity for frequencies near  $f_R$  for frequencies at the low end of the VHF<sub>LO</sub> band.

Thus receiver **700** is highly integrated and achieves low cost by using on-chip inductors. The size of the inductor in the VHF<sub>LO</sub> band can be made small by implementing a single-ended filter as an RLC filter in which the resistance is formed in part by the parasitic resistance of an on-chip inductor, and in part by a separate integrated resistor. Receiver **700** adds an additional parallel resonant LC filter bandpass with a slightly higher quality inductor to provide additional selectivity in the passband.

The above-disclosed subject matter is to be considered illustrative, and not restrictive, and the appended claims are intended to cover all such modifications, enhancements, and other embodiments that fall within the true scope of the claims. Thus, to the maximum extent allowed by law, the scope of the present invention is to be determined by the broadest permissible interpretation of the following claims and their equivalents, and shall not be restricted or limited by the foregoing detailed description.

What is claimed is:

1. A receiver comprising:

a first amplifier having an input for receiving a radio frequency signal, and an output;

a first filter having an input coupled to the output of the first amplifier, a tuning input, and an output, for substantially passing frequencies below a variable cutoff frequency, the variable cutoff frequency being less than an upper frequency threshold of the first filter;

a second filter having an input coupled to the output of the first amplifier, a tuning input, and an output, for substantially passing frequencies within a band above a lower threshold frequency of the second filter and below an upper threshold frequency of the second filter;

wherein the first filter comprises:

a first variable capacitor having a first terminal coupled to the output of the first amplifier, a second terminal coupled to a power supply voltage terminal, and a control terminal for receiving a tuning signal; and

## 14

an inductance leg having a first terminal coupled to the output of the first amplifier, and a second terminal coupled to the power supply voltage terminal, the inductance leg including a first inductor and having an effective resistance in series with the inductor, wherein the effective resistance has a value related to an upper cutoff frequency to be tuned by the first filter.

2. The receiver of claim 1, further comprising:

a resistor having a first terminal coupled to the output of the first amplifier, and a second terminal coupled to a first terminal of the inductor, wherein the effective resistance of the inductance leg is equal to a resistance of the resistor plus a parasitic resistance of the inductor.

3. The receiver of claim 1, wherein the first variable capacitor comprises:

a fixed capacitor having a first terminal coupled to the output of the first amplifier, and a second terminal coupled to the power supply voltage terminal;

a binary capacitor having a first terminal coupled to the output of the first amplifier, a second terminal coupled to the power supply voltage terminal, and a control terminal for receiving binary coded signal; and

a thermometer capacitor having a first terminal coupled to the output of the first amplifier, a second terminal coupled to the power supply voltage terminal, and a control terminal for receiving thermometer coded signal.

4. The receiver of claim 1, further comprising:

a second amplifier having an input coupled to the output of the first amplifier, and first and second outputs forming a differential signal pair;

a second variable capacitor having a first terminal coupled to the first output of the second amplifier, and a second terminal coupled to the second output of the second amplifier, and a tuning input terminal; and

a second inductor having a first terminal having a first terminal coupled to the first output of the second amplifier, and a second terminal coupled to the second output of the second amplifier.

5. The receiver of claim 1, wherein each of the upper frequency threshold of the first filter and the lower frequency threshold of the second filter is approximately equal to 190 megahertz (MHz).

6. The receiver of claim 1, further comprising:

a third filter having an input coupled to the output of the first amplifier, a tuning input, and an output, for substantially passing frequencies within a band above a lower threshold frequency of the third filter.

7. The receiver of claim 6, wherein the third filter comprises:

a third variable capacitor including a first terminal coupled to the output of the first amplifier, and a second terminal coupled to a second power supply voltage terminal; and

a transformer including a primary winding having a first terminal coupled to the first terminal of the third variable capacitor and a second terminal coupled to a third power supply voltage terminal, and a secondary winding having a first terminal and a second terminal for providing a differential filtered radio frequency signal thereto.

8. The receiver of claim 7, wherein each of the upper frequency threshold of the second filter and the lower frequency threshold of the third filter is approximately equal to 470 MHz.

\* \* \* \* \*